

微束等离子喷涂制备羟基磷灰石涂层

赵秋颖, 贺定勇, 李晓延, 栗卓新*

(北京工业大学 材料科学与工程学院, 北京 100022)

摘 要: 采用微束等离子喷涂系统制备羟基磷灰石涂层, 通过扫描电子显微分析(SEM)和 X 射线衍射分析(XRD)对涂层形貌、相组成和结晶度进行了研究。结果表明, 随着喷涂电流和离子气流量的增加, 羟基磷灰石粒子的熔化和撞击后的铺展更充分, 在 70~130 mm 范围内随着喷涂距离的增加粒子熔化程度增加。适当的喷涂工艺条件下微束等离子喷涂制备羟基磷灰石涂层的结晶度可以相当或高于传统大气等离子喷涂制备的涂层, 有利于涂层在体液环境中稳定性的提高。

关键词: 微束等离子喷涂; 羟基磷灰石涂层; 结晶度; 涂层结构

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赵秋颖

0 序 言

20 世纪 90 年代以来, 金属基体表面制备羟基磷灰石(hydroxyapatite, HA)涂层的生物植入体以其无毒、不致癌, 良好的生物相容性和力学相容性, 不引起急性中毒、溶血和过敏现象等优势而真正应用于生物体修复, 已在临床取得重要成果^[1]。大气等离子喷涂(atmospheric plasma spraying, APS)工艺制备 HA 生物涂层是目前研究最多也相对成熟的方法之一^[2,3]。作为一种高温工艺过程, APS 制备的涂层保持了 HA 的生物相容性和生物活性, 然而由于 HA 在喷涂过程中的分解和非晶相的形成, 涂层结晶度一般低于 70%^[4], 在生物负载和体液腐蚀的条件下容易分解导致涂层脱落而造成失效。对于与涂层结晶度相关问题的研究已经成为制备兼具生物活性和生物稳定性的 HA 涂层的热点问题。

目前, 乌克兰巴顿焊接所^[5]及德国亚琛工业大学^[6]等少数研究单位首先采用微束等离子喷涂技术(micropasma spray, MPS)在制备生物陶瓷涂层方面开展了一些研究工作。北京工业大学^[7]研制的 WDP-1 型微束等离子喷涂系统采用氩气作为工作气, 焰流的功率仅为 1~2 kW, 具有焰流为层流、阳极直径小、能量集中等特点, 可以节约喷涂材料。

并且仅通过调整喷涂工艺参数就能获得结晶度不同的 HA 涂层, 适当的工艺参数可以直接获得结晶度高于 85%的涂层。作者采用 MPS 工艺制备 HA 涂层, 研究喷涂工艺参数对涂层表面形貌、相组成和结晶度的影响规律。

1 试验方法

基体材料选用 Ti6Al4V, 规格为 $\phi 15 \text{ mm} \times 3 \text{ mm}$, 喷涂前预先进行喷砂粗化处理, $R_a=9.0 \sim 12.0 \mu\text{m}$, 置于丙酮中进行超声波清洗; 喷涂材料选用山东大学新材料中心提供的粒度为 50~80 μm 的 HA 粉末, 钙磷摩尔比为 1.67。

采用 WDP-1 型微束等离子喷涂系统制备 HA 涂层。该系统在喷嘴外安装了一个可拆卸的阳极, 粉末从阳极和喷嘴之间的空隙中加入。由于采用外置阳极, 等离子弧几乎不受压缩和旋转作用, 能在阳极稳定的燃烧。为研究工艺参数对 HA 涂层特性的影响, 采用喷涂电流范围为 30~50 A、喷涂距离为 70~130 mm、喷涂气流量为 0.8~1.5 L/min。具体工艺参数如表 1 所示。

采用 FEI Quanta 200 扫描电子显微镜观察涂层的表面形貌。利用 D8 ADVANCE X 射线衍射仪检测相组成, 铜靶($K\alpha$), 测量范围 $25^\circ \sim 60^\circ$, 扫描速度 $0.02^\circ/\text{s}$ 。并根据 X 射线衍射图谱, 采用曲线拟合非晶峰法^[8], 计算涂层结晶度, 用作定性分析, 以探讨不同工艺参数对于结晶度的影响规律。

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*参加此项研究工作的还有蒋建敏

表 1 微束等离子喷涂参数
Table 1 Microplasma spraying parameters

样品 编号	喷涂电流 I/A	喷涂距离 d/mm	喷涂气流量 $Q/(\text{L}\cdot\text{min}^{-1})$
1	45	70	1.1
2	45	100	1.1
3	45	130	1.1
4	35	70	1.1
5	50	70	1.1
6	60	70	1.1
7	45	70	0.8
8	45	70	1.5

2 试验结果与讨论

2.1 喷涂工艺参数对涂层表面形貌的影响

2.1.1 喷涂距离对涂层表面形貌的影响

图 1 是将 HA 粉末在喷涂电流 45 A、不同喷涂

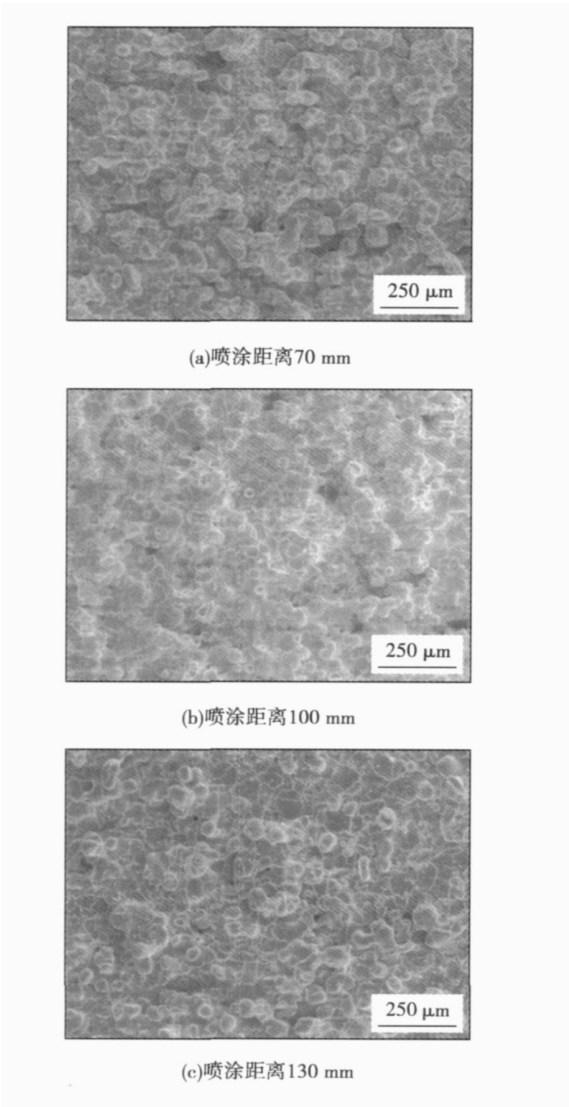


图 1 不同喷涂距离下涂层的表面形貌
Fig. 1 Surface morphology of MPS coatings with difference distance

距离下喷涂所获得涂层的表面形貌。涂层主要是由熔化较为充分的直径约为 20~50 μm 的饼状或不规则球状的 HA 颗粒相互重叠和粘结而成,有少量孔隙,表面较为致密。根据涂层表面颗粒的形态可以看出,涂层颗粒都得到了充分熔化。微束等离子射流的速度在喷嘴处最高。沿射流方向,射流速度随距离的增加而减小。使喷涂粒子先是被加速,后又随喷涂距离的增加而速度降低,动能减小。由图 1 看出,随着喷涂距离的增大,涂层表面颗粒的扁平化程度减小,其形状由扁平状逐渐变为扁球状。

此外,涂层表面粘附有部分直径约为 2~10 μm 细小的球形颗粒。这些小颗粒部分来源于熔融颗粒在飞行过程中发生的破碎,部分来源于熔融颗粒到达基体后给基体以很大的冲力,在基体反作用力的作用下产生的飞溅。

2.1.2 喷涂电流对涂层表面形貌的影响

图 2 是喷距为 70 mm 时,采用不同喷涂电流所得到涂层的表面形貌。可以看出,随喷涂电流的提高,涂层中颗粒的变形度明显提高。在 35 A 的喷涂电流下,涂层中颗粒熔化程度较低,可见大量残留大颗粒,变形不太充分,涂层片状堆积不太紧密。在 50 A 的喷涂电流下,电弧的温度明显升高,涂层颗粒熔化程度较高,变形充分,涂层表面较为平整,涂层边缘有明显溅射的痕迹。因此,在该喷涂距离下,

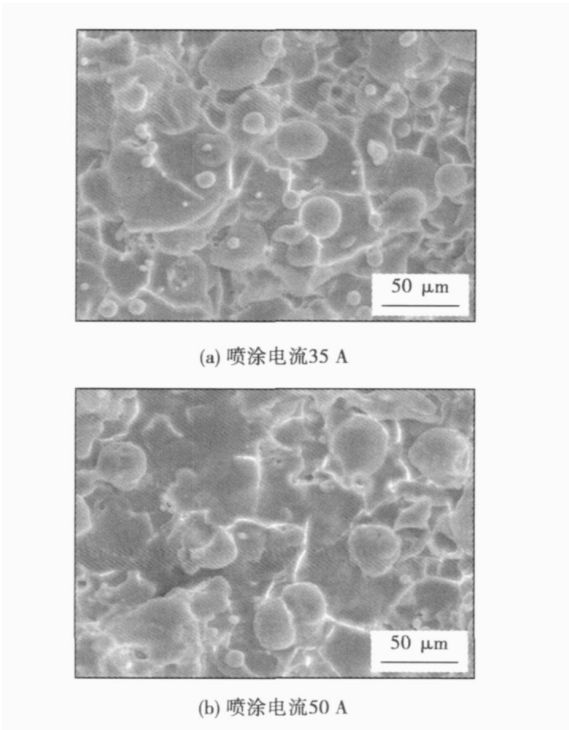


图 2 不同喷涂电流下涂层的表面形貌
Fig. 2 Surface morphology of MPS coatings with difference current

提高喷涂电流可明显提高颗粒的熔化程度。

熔化程度的提高有利于涂层本身及其与基体的结合强度, 但过分熔化将导致涂层结晶度下降, 表面粗糙度降低, 影响种植体在体液中的稳定性, 减缓新骨的生长速度。

2.1.3 喷涂气流量对涂层表面形貌的影响

图 3 是喷涂距离为 70 mm、喷涂电流为 45 A 条件下, 采用不同气流量喷涂 HA 涂层的表面形貌。在 0.8 L/min 气流量的条件下, 涂层表面有大量圆球状颗粒, 堆积不紧密, 存在一定的孔隙。这是因为在低气流量条件下, 颗粒的速度较低, 对基体的碰撞作用降低, 在等离子焰流中滞留时间变长, 熔化量较大。而在 1.5 L/min 气流量的条件下, 涂层表面较为平坦, 涂层粒子堆积紧密, 孔隙不太明显, 存在明显未熔化的大颗粒。

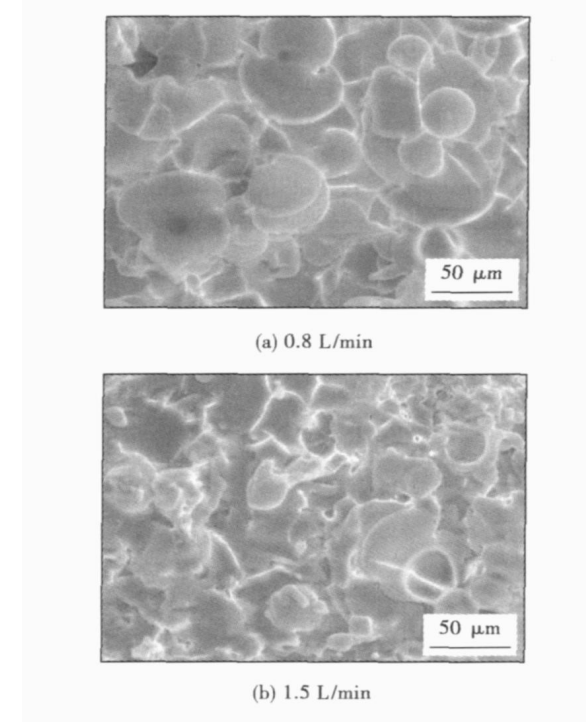


图 3 不同喷涂气流量下涂层的表面形貌
Fig. 3 Surface morphology of MPS coatings with different gas flow rate

喷涂过程采用高气流量参数相比较低的气流量条件, HA 颗粒的飞行速度较高, 在等离子焰流中的滞留时间变短, 颗粒温度低, 熔化量减少。同时粒子加速程度高, 撞击基体时的碰撞作用增加, 一方面了提高涂层的致密度; 另一方面增加了颗粒的反弹损失, 沉积率下降。

2.2 喷涂工艺参数对涂层相组成和结晶度的影响
结晶度这一参数对涂层的稳定性有双重的影

响, 结晶度越高涂层越稳定, 但对生物活性有所损害, 因此涂层的结晶度要同时满足稳定性和生物活性的双重要求, 并不是越高越好。

GROSS 等人^[9] 研究发现, 促使非晶相形成的最主要因素是: 熔化的 HA 粒子在热过程中的脱羟基反应, 撞击基体材料过程中的冷却速率以及基体的温度。因此调整不同的喷涂参数可以控制涂层中的非晶态的含量。

2.2.1 喷涂距离对涂层相组成和结晶度的影响

图 4 为喷涂电流为 45 A, 不同喷涂距离下制备 HA 涂层的 X 射线衍射图。可以看出, 喷涂距离对涂层的相组成未产生显著影响。1, 2 和 3 号涂层的结晶度经计算分别为 90.2%, 88.0%和 65.2%。

涂层主要是由 HA 晶相、少量非晶相及少量 α-磷酸钙 (α-tricalcium phosphate, α-TCP) 和 β-磷酸钙 (β-tricalcium phosphate, β-TCP) 等亚稳态磷酸钙化合物组成, 三种涂层的 α-TCP、β-TCP 和非晶相的含量略有不同。各个喷涂距离下涂层中并未存在非生物活性的杂质相氧化钙 (CaO) 和易在体液条件溶解的四磷酸钙 (tetra calcium phosphate, TTCP)。在体液环境下, 涂层组成物的溶解速度为 ACP >> TTCP > α-TCP > β-TCP >> HA, 因而从相组成来说, MPS 制得的 HA 涂层易溶解相含量低, 有利于生物涂层的稳定。

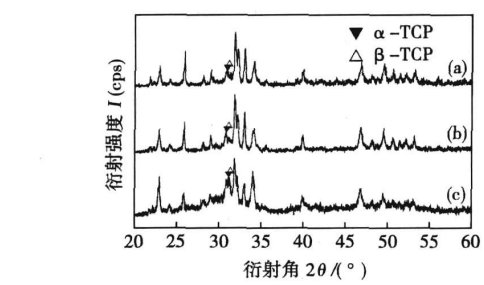


图 4 不同喷涂距离下 HA 涂层的 X 射线衍射图 (a) 70 mm (b) 100 mm, (c) 130 mm

Fig. 4 X-ray diffraction spectra at 45 A and different distances of (a) 70 mm, (b) 100 mm, and (c) 130 mm

2.2.2 喷涂电流对涂层相组成和结晶度的影响

图 5 为喷涂距离为 70 mm 时不同喷涂电流下制备 MPS 涂层的 X 射线衍射图。

随喷涂电流的提高, HA 晶相衍射三强线的衍射强度逐渐减小, 其余衍射线逐渐减弱甚至消失, 涂层非晶化程度提高。分析可知, 一方面, 随喷涂电流的提高, 等离子焰流和颗粒的温度随之增加, 所以颗粒熔化部分增多, 氧羟基磷灰石 (oxyhydroxyapatite, OHA) 随之增多。另一方面, 等离子焰流和熔滴的热

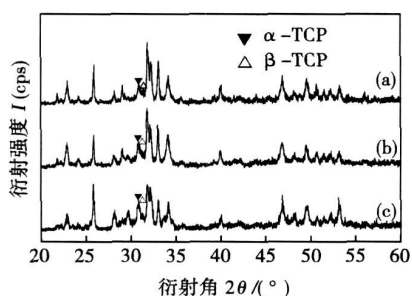


图 5 不同喷涂电流下 MPS 涂层的 X 射线衍射图 (a) 35 A (b) 50 A (c) 60 A

Fig. 5 X-ray diffraction spectra at 70mm and different current of (a) 35 A (b) 50 A, and (c) 60 A

聚集作用也导致基体的温度增加,所以冷却速度变慢,这将引起更多的 OHA 和已经形成的非晶部分的再结晶。但由于颗粒熔化部分增多,冷却形成的非晶占主导地位,所以总的结果是电流增大,杂质相增多,结晶度降低,而且结晶相主要以再结晶的为主。

3 讨 论

微束等离子喷涂 HA 涂层的表面形貌、相组成和结晶度可以通过调整工艺参数来控制。采取适当的工艺参数,不经过后热处理涂层的结晶度可以达到 90% 以上。MPS 工艺本身的特性应是使得涂层结晶度高,有害杂质少的本质原因。

首先,MPS 采用的工作气体为氩气,无辅助气体。等离子体的热传导较低,有利于减少 HA 粉末的温度梯度,减轻粉末过热,因而 HA 粉末分解并不严重,杂质含量少;第二,MPS 粒子的速度低。喷涂速度低使粉末在焰流的停留时间长,有利于粉末温度梯度的降低,利于 HA 趋向平衡反应,可促使杂质相向 OHA 转变;第三,微束等离子体的功率和气流量之比(5~20)大于常规等离子(0.5~1.0),有利于粉末的均匀加热。

4 结 论

(1) 微束等离子喷涂 HA 涂层的显微结构和相

组成受喷涂距离、电流、气流量等喷涂工艺参数的影响。单一增加喷涂距离或电流均能导致颗粒熔化增加,涂层的结晶度下降;增加气流量导致颗粒熔化减少,涂层的结晶度升高。微束等离子涂层制备的高结晶度涂层其结晶度($> 90\%$)高于大气等离子制备的高结晶度涂层($< 80\%$)。通过调整工艺参数,也可方便地制备结晶度较低($< 70\%$)的涂层。

(2) 微束等离子喷涂 HA 涂层不含杂质相 CaO 和 TiCP 等,其主要原因是 MPS 功率低、喷涂速度低及采用导热低的纯氩气。

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作者简介: 赵秋颖,女,1983 年出生,博士研究生。研究方向为微束等离子喷涂制备生物涂层。

Email: zhaoqiuying@emails.bjut.edu.cn

Data fusion of multi-sensor in container NC welding machine

CHEN Lihua¹, TIAN Songya², ZHANG Genyuan², SHI Rusheng², ZHU Xiaohua² (1. Changzhou Institute of Mechatronic Technology, Changzhou 213164, Jiangsu, China; 2. Hohai University, Changzhou 213022, Jiangsu, China). p133—136

Abstract: Container NC welding machine includes multi-sensor system, computer control system and step motor drive system. Data process in multi-sensor is the key part of this machine. Container floor and the sidewall weld is broken line. For the weld is 12 meters long and allowance exists in machine and fix, and welding induces deformation, therefore automatic welding must take action of the seam track. The multi-sensor system consists of laser sensor and high-precision ultrasonic sensor, for straight bead ultrasonic sensor controls the distance from welding torch to side wall. While for the turn corner bead the system uses expert system for data fusion of two sensor signals and a final decision is made. Torch position can be adjusted in order to weld continuously. It can also provide a theoretical foundation for the various curves seam tracking study in the future.

Key words: container; numerical control welding machine; multi-sensor; data fusion

Microplasma arc sprayed hydroxyapatite coatings

ZHAO Qi-uying, HE Dingyong, LI Xiaoyan, LI Zhuoxin, JIANG Jianmin (School of Materials Science and Engineering, Beijing University of Technology, Beijing 100022, China). p137—140

Abstract: Microplasma arc spraying was utilized to deposit hydroxyapatite(HA) powders on Ti6Al4V substrate. Scanning electron microscope and X-ray diffraction were used to investigate the morphology, phase, and crystallinity of the HA coatings. Sufficient melting of HA particles and spreading after collision were observed with the increase of arc current and gas flow rate. Within the spraying distance range from 70 mm to 130 mm, the degree of melting of the HA particles increased with the spraying distance. Under appropriate spraying parameters the crystallinity of microplasma arc sprayed HA coatings was comparable or even higher than the one from conventional atmospheric plasma arc spraying, which is beneficial to the improvement of their stabilities in such liquid environment as body fluids.

Key words: microplasma arc spraying; hydroxyapatite coating; crystallinity; coating structure

Automatic underwater arc welding seam-tracking system based on flux-core wire and rotating arc sensor

YE Jianxiang¹, ZHANG Hua² (1. Department of Mechanical Engineering, Nanchang Institute of Technology, Nanchang 330099, China; 2. Key Laboratory of Robot & Welding Automation, Nanchang University, Nanchang 330031, China). p141—144

Abstract: The wet underwater arc welding seam-tracking technology based on rotating arc sensor is introduced. An experimental system used to study the welding automation is established and

welding parameters are found out at first for flux core arc welding based on experiments. The approach of calculating the welding current integration differences is adopted here to determine the welding-gun horizontal bias and vertical bias. Manifold digital signal process methods are performed on all sampled noisy signals to improve stability and reliability of results. Analysis on massive experimental data revealed that both horizontal bias and vertical bias can all be clarified clearly by this way. Furthermore, a manipulating system is carried out on above conclusions, and two kinds of different manipulators—Fuzzy controller and hybrid PID controller are designed separately to adjust the horizontal deviation and vertical deviation. The results of verifying tests approved the effectiveness of all above work.

Key words: rotating arc welding sensor; wet underwater welding; area integration method; seam-tracking

Microstructures of high chromium cast iron for surfacing

WEI Jianjun, HUANG Zhiqian, YANG Wei (Zhengzhou Research Institute of Mechanical Engineering, Zhengzhou 450001, China). p145—148

Abstract: The flux-cored wires with different contents of carbon and chromium for submerged arc welding is designed, which composition range of surfacing metal is 4.0%—6.5% C and 20%—40% Cr. Different analysis methods such as metallographic test, MPMA, the hardness test were utilized to analyse the influence for microstructures, hardness, qualities and distribution of primary carbide with different contents of C, Cr and Cr/C.

Key words: high chromium cast iron; flux-cored wires; primary carbide

Horizontal welding of pulsed submerged arc welding and its application in oil tank manufacturing

GAO Ying^{1,2}, LI Huan^{1,2}, SUN Bo^{1,2}, YANG Zhansheng^{1,2} (1. School of Materials Science and Engineering, Tianjin University, Tianjin 300072, China; 2. Tianjin Key Laboratory of Advanced Joining Technology, Tianjin 300072, China). p149—152

Abstract: In order to analyze the stress situation of the molten pool in horizontal pulsed SAW (submerged arc welding), the pool was simplified into a piece of liquid metal on the surface of solid metal, which receives pulse load regularly. In this way, the mechanism of undercut elimination with pulse current was brought forward, i.e., the arc force loaded to the pool, the impact force of droplet transfer and the resultant surface tension all follow the regular pulse current change. Such regular change of these forces helps to eliminate the undercut. The forces follow the regular changes of pulse current, and the peak value of certain pulse current ensures a pleasant penetration to prevent incomplete penetration. The pulse current can also restrain the undercut. Therefore, the range of processing parameters in ordinary horizontal SAW can be increased with the technology of pulse horizontal SAW.

Key words: pulsed submerged arc welding; oil tank; horizontal welding; undercut